

Turbulence generation by planar detonations in heterogeneous mixtures

Workshop on Fluid Dynamics 2019

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Detonation Turbulence Phenomena

Description of the problem

1D Reactive Rankine-Hugoniot relation

Effect of local perturbations in the fuel mass fraction

Qualitative analysis

Mathematical model

Non-dimensional governing equations

Linearized Reactive Rankine-Hugoniot Equations

Problem domain and boundary conditions

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Here we are dealing with two different phenomena which are, independently, very complex to model: Detonations & Turbulence.

Therefore, strong simplifications must be done in order to get an analytically tractable problem

- ▶ **Detonation:** planar and **stable**.
- ▶ **Turbulence:** weak, homogeneous and isotropic¹.

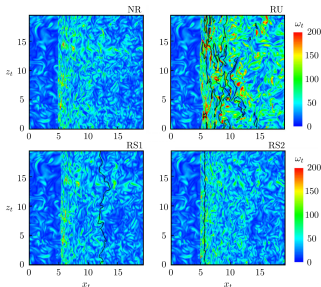


Figure 1: Instantaneous vorticity patterns for NR, RU, RS1, and RS2 obtained at the cut plane $y_t = (6.61\pi)/2$. Black contour lines on the reactive cases correspond to the isolines of nearly complete depletion of reactant $Y = 0.01$ (Huete 2017).

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¹G. Keith Batchelor. The theory of homogeneous turbulence. Cambridge university press, 1953.

Definitions

- density:

$$\rho = \rho_o (1 + W\hat{Y}), \quad (1)$$

- heat release:

$$q = q_o (1 + H\hat{Y}), \quad (2)$$

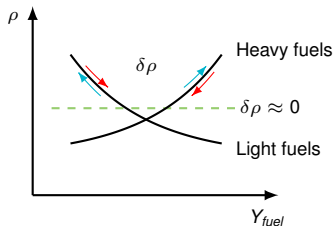
- mixture ratio:

$$W = \frac{1 - \frac{W_{air}}{W_{fuel}}}{Y_{fuel} + \frac{W_{air}}{W_{fuel}}(1 - Y_{fuel})}. \quad (3)$$

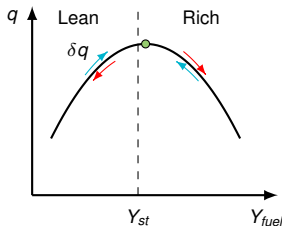
■ constructive

■ destructive

■ non-effect



(a)



(b)

Figure 2: Variation of mixture density (a) and heat release (b) with the fuel mass fraction and the equivalence ratio.

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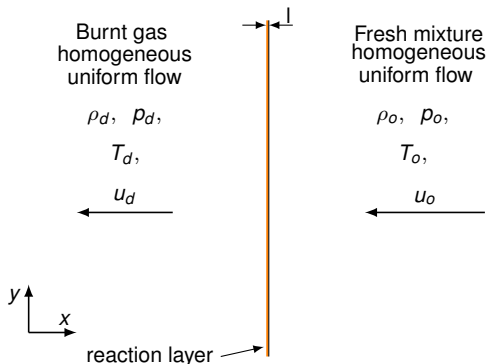


Figure 3: Sketch of the planar detonation front, where l is the thickness of the reaction layer. Reference frame moving with the shock surface.

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$$\frac{\rho_d}{\rho_o} = \frac{(\gamma+1)\rho_d - (\gamma-1)\rho_o + 2(\gamma-1)\rho_d \rho_o q / \rho_o}{(\gamma+1)\rho_o - (\gamma-1)\rho_d}$$

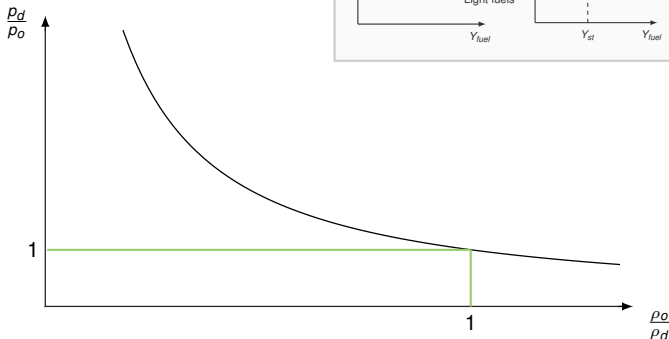


Figure 4: Perturbations on the Rankine-Hugoniot relation.

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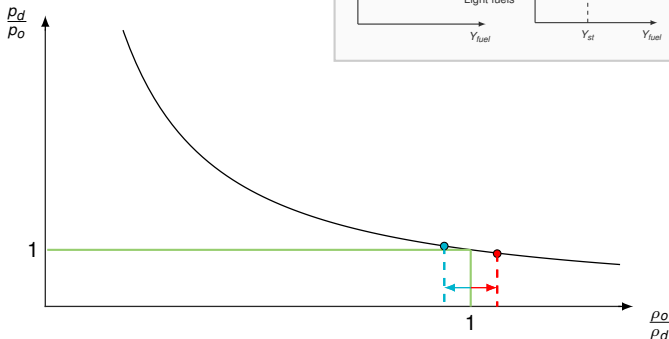


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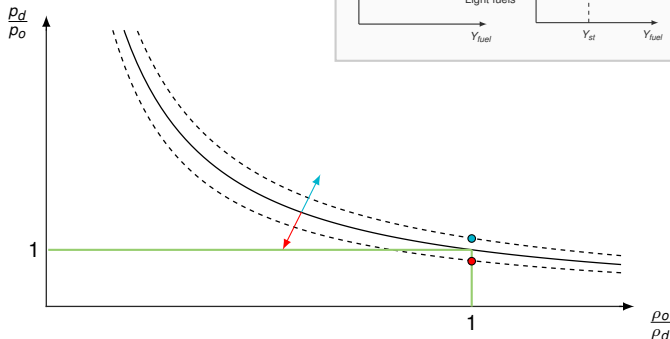


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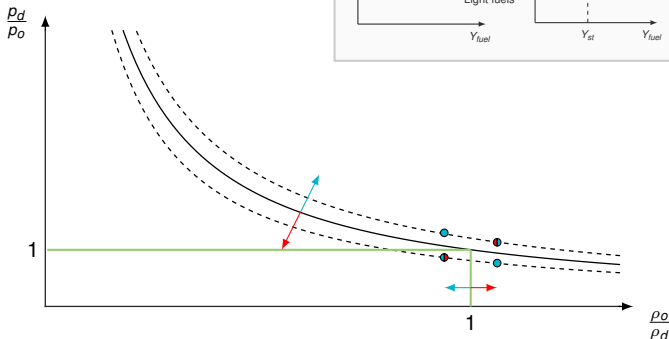


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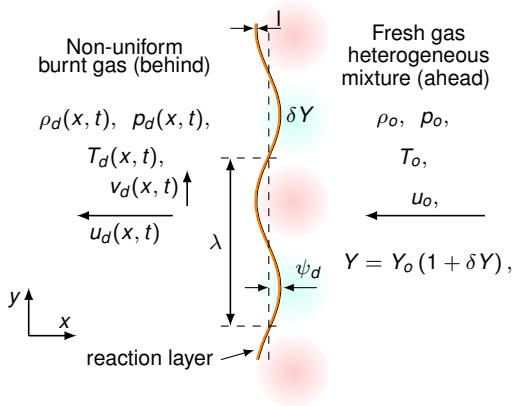


Figure 5: Sketch of the corrugated detonation front, where ψ_d is the amplitude of the detonation shape deviations respect to the planar shape, and must satisfy $l \ll \psi_{d0} \ll \lambda$. Reference frame moving with the shock surface.

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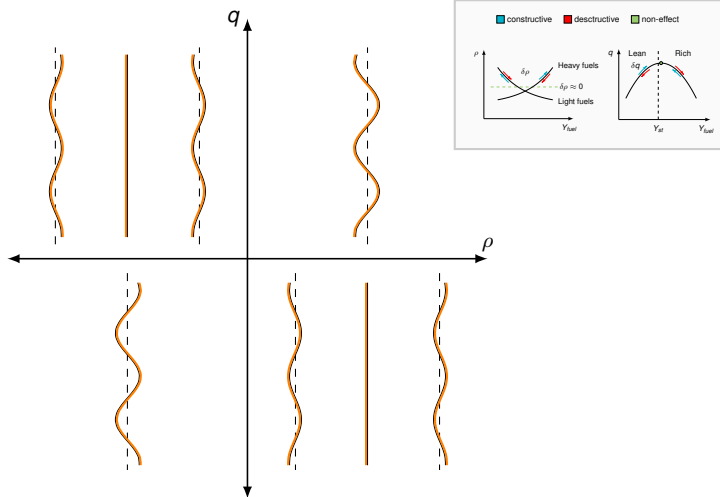


Figure 6: Qualitative analysis between the heat release and the mixture density.

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- ▶ Perfect gases.

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- ▶ Perfect gases.
- ▶ Thin detonation limit: **The detonation wave is treated as a pure discontinuity**². Infinitely fast chemistry, $Da \gg 1$ in order to satisfy $l \ll \xi$.

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- ▶ Thick detonation limit: The size of the perturbations is much smaller than the detonation thickness³. **Linear theory**, $\xi \ll \lambda$.

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- ▶ Isotropic probability density function (**analysis of all the spectrum**).

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- ▶ Thick detonation limit: The size of the perturbations is much smaller than the detonation thickness³. **Linear theory**, $\dot{\xi} \ll \lambda$.
- ▶ Isotropic probability density function (**analysis of all the spectrum**).

The functions of interest are perturbed, namely

$$\hat{p}(\hat{x}, \tau) = \hat{\rho}_a(\hat{x}, \tau) = \mathbb{P}e^{i(\hat{\omega}\tau - \hat{k}\hat{x})} e^{i\hat{y}}, \quad (4)$$

$$\hat{\rho}(\hat{x}, \tau) = \hat{\rho}_a + \hat{\rho}_e, \quad (5)$$

$$\hat{u}(\hat{x}, \tau) = \hat{u}_a + \hat{u}_r, \quad (6)$$

$$\hat{v}(\hat{x}, \tau) = \hat{v}_a + \hat{v}_r, \quad (7)$$

for the pressure, density, longitudinal velocity and transverse velocity, respectively.

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Non-dimensional compressible Euler equations:

$$\frac{\partial \hat{p}}{\partial \tau} + \frac{\partial \hat{u}}{\partial \hat{x}} + \frac{\partial \hat{v}}{\partial \hat{y}} = 0, \quad (8a)$$

$$\frac{\partial \hat{u}}{\partial \tau} + \frac{\partial \hat{p}}{\partial \hat{x}} = 0, \quad (8b)$$

$$\frac{\partial \hat{v}}{\partial \tau} + \frac{\partial \hat{p}}{\partial \hat{y}} = 0, \quad (8c)$$

$$\frac{\partial \hat{p}}{\partial \tau} - \frac{\partial \hat{p}}{\partial \tau} = 0, \quad (8d)$$

can be linearly manipulated to give:

$$\frac{\partial^2 \hat{p}}{\partial \tau^2} = \frac{\partial^2 \hat{p}}{\partial \hat{x}^2} + \frac{\partial^2 \hat{p}}{\partial \hat{y}^2}. \quad (9)$$

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Non-dimensional compressible Euler equations + **periodically symmetric condition**:

$$\frac{\partial \hat{\rho}}{\partial \tau} + \frac{\partial \hat{u}}{\partial \hat{x}} + \hat{v} = 0, \quad (8a)$$

$$\frac{\partial \hat{u}}{\partial \tau} + \frac{\partial \hat{p}}{\partial \hat{x}} = 0, \quad (8b)$$

$$\frac{\partial \hat{v}}{\partial \tau} - \hat{p} = 0, \quad (8c)$$

$$\frac{\partial \hat{p}}{\partial \tau} - \frac{\partial \hat{p}}{\partial \tau} = 0, \quad (8d)$$

Two-dimensional **periodically symmetric** wave equation for the burnt gas:

$$\frac{\partial^2 \hat{p}}{\partial \tau^2} = \frac{\partial^2 \hat{p}}{\partial \hat{x}^2} - \hat{p}. \quad (9)$$

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The perturbations behind the shock (one of the boundary conditions) are given by the linearized Rankine-Hugoniot equations

$$\frac{D\xi_d}{D\tau} = \frac{R_d}{R_d - 1} \left[\frac{1 + \Gamma_d}{2M_d} \hat{p}_d + \frac{M_d}{2} (W(2 - R_d) - \Delta_d) \frac{M_d}{2} \hat{Y} \right], \quad (10a)$$

$$\hat{u}_d = \frac{1 + \Gamma_d}{2M_d} \hat{p}_d + \frac{M_d}{2} (\Delta_d - R_d W) \hat{Y}, \quad (10b)$$

$$\hat{v}_d = M_d(R_d - 1) \frac{\partial \xi_d}{\partial \hat{y}}, \quad (10c)$$

$$\hat{p}_d = \frac{\Gamma_d}{M_d^2} \hat{p}_d + \Delta_d \hat{Y}, \quad (10d)$$

where ξ_d is the dimensionless shock ripple amplitude, and Γ_d and Δ_d are the Rankine-Hugoniot slope and the heat release contribution, both downstream, respectively.

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Combining RH-equations with conservation equations we get:

$$a_1 \frac{\partial^2 \hat{p}_d}{\partial \tau^2} + a_2 \frac{\partial^2 \hat{p}_d}{\partial \tau \partial \hat{x}} + a_3 \frac{\partial^2 \hat{p}_d}{\partial \hat{x}^2} + a_4 \frac{\partial^2 \hat{p}_d}{\partial \hat{y}^2} = f(\hat{\omega}_s), \quad (11)$$

where a_1 , a_2 , a_3 , and a_4 are constants, and $f(\hat{\omega}_s)$ is a function that depends of the shock frequency.

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where a_1 , a_2 , a_3 , and a_4 are constants, and $f(\hat{\omega}_s)$ is a function that depends of the shock frequency.

Assuming

$$\hat{p} = \mathbb{P} e^{i(\hat{\omega}\tau - \hat{k}\hat{x})}, \quad (12)$$

which satisfy the wave equation (9), and in order to apply normal modes

$$\hat{Y}_s = e^{i(\hat{\omega}_s \tau + \hat{y})}, \quad (13)$$

which gives

$$\hat{\omega}^2 = \hat{k}^2 + 1, \quad (14)$$

$$\hat{\omega}_s = \hat{\omega} - \hat{k}M_d, \quad (15)$$

where $\hat{\omega}$ and $\hat{\omega}_s$ are the dimensionless frequency and the dimensionless shock frequency, respectively.

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$$\left[-\hat{\omega}_s^2 \sigma_b - \hat{\omega}_s \sqrt{\hat{\omega}_s^2 + M_d^2 - 1} - M_d^2 (R_d - 1) \sigma_a \right] \mathbb{P} e^{i(\hat{\omega}_s \tau)} = f(\hat{\omega}_s) e^{i\hat{\omega}_s \tau}, \quad (16)$$

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$$\left[\zeta \sigma_b + \zeta \sqrt{\zeta^2 - 1} (1 - M_d^2)^{-1/2} - \sigma_c \right] \mathbb{P} e^{i\hat{\omega}_s \tau} = f^*(\hat{\omega}_s) e^{i\hat{\omega}_s \tau}, \quad (17)$$

with

$$\zeta = \frac{\hat{\omega}_s}{\sqrt{1 - M_d^2}}. \quad (18)$$

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$$\left[\zeta \sigma_b + \zeta \sqrt{\zeta^2 - 1} (1 - M_d^2)^{-1/2} - \sigma_c \right] \mathbb{P} e^{i\hat{\omega}_s \tau} = f^*(\hat{\omega}_s) e^{i\hat{\omega}_s \tau}, \quad (17)$$

with

$$\zeta = \frac{\hat{\omega}_s}{\sqrt{1 - M_d^2}}. \quad (18)$$

► $\zeta > 1$:

$$\mathbb{P} = \frac{f^*(\hat{\omega}_s)}{\zeta \sigma_b + \zeta \sqrt{\zeta^2 - 1} (1 - M_d^2)^{-1/2} - \sigma_c}. \quad (19)$$

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Dispersion relation:

$$\left[-\hat{\omega}_s^2 \sigma_b - \hat{\omega}_s \sqrt{\hat{\omega}_s^2 + M_d^2 - 1} - M_d^2 (R_d - 1) \sigma_a \right] \mathbb{P} e^{i(\hat{\omega}_s \tau)} = f(\hat{\omega}_s) e^{i\hat{\omega}_s \tau}, \quad (16)$$

$$\left[\zeta \sigma_b + \zeta \sqrt{\zeta^2 - 1} (1 - M_d^2)^{-1/2} - \sigma_c \right] \mathbb{P} e^{i\hat{\omega}_s \tau} = f^*(\hat{\omega}_s) e^{i\hat{\omega}_s \tau}, \quad (17)$$

with

$$\zeta = \frac{\hat{\omega}_s}{\sqrt{1 - M_d^2}}. \quad (18)$$

► $\zeta > 1$:

$$\mathbb{P} = \frac{f^*(\hat{\omega}_s)}{\zeta \sigma_b + \zeta \sqrt{\zeta^2 - 1} (1 - M_d^2)^{-1/2} - \sigma_c}. \quad (19)$$

► $\zeta < 1$:

$$\text{Re} \left\{ \mathbb{P} e^{i\hat{\omega}_s \tau} \right\} = a \cos(\hat{\omega}_s \tau) + \sin(\hat{\omega}_s \tau). \quad (20)$$

Turbulence generation by planar detonations in heterogeneous mixtures

A. Cuadra-Lara,
C. Huete & M. Vera

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1D Reactive Rankine-Hugoniot relation
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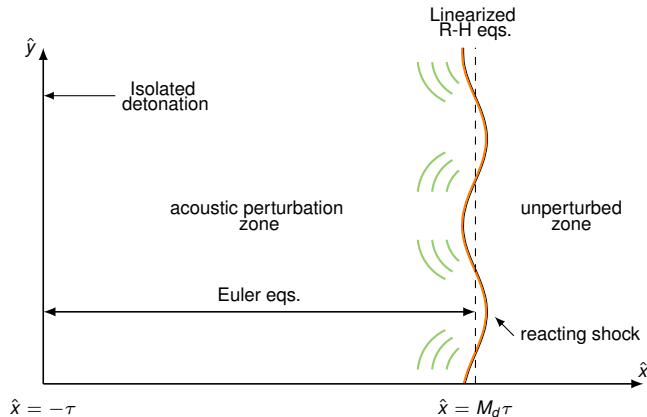
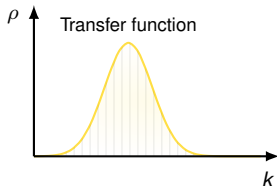


Figure 7: Problem domain and boundary conditions. Reference frame moving with the burnt gas.

- ▶ Downstream averages (Velikovich, 2012). Superposition of the modes (linear theory).



- ▶ Characterize the turbulence generated by a given dispersion relationship in the heterogenous mixture.
- ▶ Evaluate how the propagation velocity and average values downstream are affected with respect to the homogenous case.
- ▶ Multiphase (droplets and high energy materials).

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Development and validation of a new MATLAB®/GUI based thermochemical code, A. Cuadra-Lara & M. Vera.

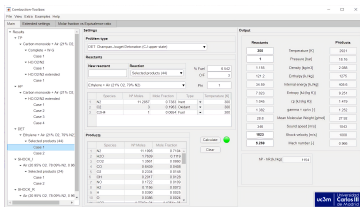


Figure 8: Current state of the GUI Combustion-Toolbox developed.

Development and validation of a new MATLAB/GUI based thermochemical code

Alberto Cuadra-Lara & Marcos Vera
Department of Thermal and Fluids Engineering, Universidad Carlos III de Madrid
28911 Getafe (Spain), 28040 Madrid (Spain), 28040 Madrid (Spain)

In this paper, a new thermochemical code is presented. The code is based on the use of the Chemkin input files and the Chemkin solver. The code is designed to be used as a stand-alone application or as a library for other applications. The code is written in MATLAB and is easy to use. The code is designed to be used as a stand-alone application or as a library for other applications. The code is written in MATLAB and is easy to use.

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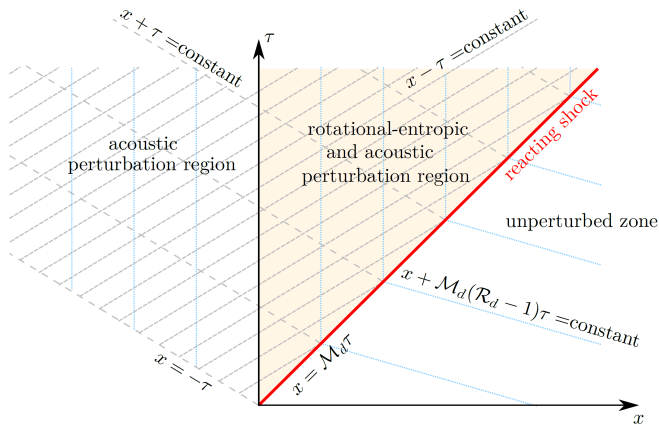


Figure 9: Integration domain and distinguished regions. Blue dotted lines refer to the particle paths, grey dashed lines indicate the positive and negative characteristic paths, respectively, and the red solid line defines the detonation trajectory (Huete 2019).

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